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UNIVERSIDAD EAFIT
THESIS OF MASTER IN SCIENCE

JOURNAL ARTICLE ON:

Computational Geometry Application in Parametric Modeling

Master Student
Samuel Vélez Sanín

Supervisor
Prof. Dr. Ing. Oscar E. Ruiz Salguero
Laboratory of CAD CAM CAE
Universidad EAFIT

Co-supervisor
Dr. Ing. Jorge Eduardo Correa Panesso
Industry and Cloud Computing in Computer Graphics
Manufactura Cohesiva S.A.S.

Dissertation
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Dedication

To my Lord and Savior, family, and friends.

Acknowledgments

Oh, the depth of the riches and wisdom
and knowledge of God! How unsearchable
are his judgments and how inscrutable his
ways!

Romans 11:33. ESV

To my Lord and Savior Jesus Christ, who gave me life, forgave my sins, and made me righteous before God: I owe you everything. Thank you for your abounding grace and mercy, for giving me the possibility to study for an MSc. degree, and for sustaining me through every step of the way.

To my Father, Mother, and Sister, thanks for your love, kindness, wisdom, and support. I could have not completed this journey without your help. Thank you for taking the time to listen to me and counsel me in hard times.

To my Grandparents, those who are with me today and those who have passed away. Thank you for your kindness, love, patience, inspiration, and taking care of me when I needed it. Certainly, without your help, this could have not been possible. This is to honor Memo, Tala and in loving memory of Pacho and Chia.

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Contents

1	Introduction	1
1.1	Summary of the Manuscript	1
1.2	List of Co-authors of the Journal Article	2
1.3	Projects	2
1.4	Distinctions	3
1.5	Academic Impact	3
1.6	How to Read this Document	4
2	Parametric Modeling of Digital Mannequins	5
2.1	Introduction	6
2.1.1	Context.	6
2.1.2	Research Strategy and Scope	7
2.1.3	Manuscript Structure.	7
2.2	Literature Review	8
2.2.1	Non-Convex Example-Based Modeling	8
	Deformation of a Single Template/Example Model	8
	Synthesis through Multiple Example Models.	9
	Feature Extraction from Photographs	10
2.2.2	Anatomy-Based Modeling	11
2.2.3	Conclusions of Literature Review	12
2.3	Materials and Methods	14
2.3.1	Rationale for the Mathematical Model	16
2.3.2	Creation of the Convex Volume Approximation	18
2.3.3	Construction of Reference Mannequins Based on the Base Mannequin	22
2.3.4	Cleaning of Reference Mannequin Geometries	24
2.3.5	Extraction of Tailor Measurements from Models	28
2.3.6	Synthesis of Mannequins from Tailor Measurements.	29
2.4	Results.	32
2.4.1	Measurement-driven Models Generated via Interpolation	32
2.4.2	Quantitative Comparison: Cushion-Based Mannequin vs. Mesh-Based Model	35
2.4.3	Interaction Simulation between Convex Volume Model and Garment	36
2.5	Conclusions and Future Work	37
3	Conclusions	40
	Bibliography	42

List of Figures

2.1	Flow diagram of the convex-volume-based measurement-driven approximation. Input: Reference 3D model. Output: Measurement-driven mannequin B . Steps 1 and 2 pre-processing. Steps 3 and 4 are processing.	16
2.2	Reference 3D model to be approximated by convex volumes. Planar data (red lines).	18
2.3	Approximation of the left thigh and hip with ellipsoids, front and lateral views. Red dotted line: surface boundary to approximate. (a) Approximation with one ellipsoid. (b) Improvement of the approximation with a second ellipsoid.	19
2.4	Approximation of the reference 3D model with ellipsoids with resulting Base Mannequin (BM) and ellipsoid mannequin and no cushions computed. (a) Half of the body approximated. (b) The full body approximated and mirroring executed.	20
2.5	Map used to convert ellipsoids into cushions, topology map and ellipsoid model. Pairs of ellipsoids with same color form a cushion.	21
2.6	Example of cushion $C_{E_1 E_2}$, arbitrarily oriented and positioned ellipsoids (E_1 and E_2) in space with convex hull operation between E_1 and E_2 . (a) Ellipsoids E_1 and E_2 . (b) Cushion $C_{E_1 E_2}$ between ellipsoids E_1 and E_2	22
2.7	Mannequin approximated with cushions and ellipsoids. Ellipsoid mannequin (a) for comparison. Cushions computed according to Figure 2.5. Small chubby mannequin (see Section 2.3.3) as (a) Ellipsoid-based Mannequin and (b) Cushion-based Mannequin.	22
2.8	Flow diagram for the construction of RM based on BM . Process for a single $RM_i \in RM$	24
2.9	Set RM of Reference Mannequins as ellipsoid mannequins (no cushions) of extreme and average models. From left to right: Small Chubby, Small Slim, Average, Tall Slim, and Tall Chubby.	24
2.10	Anatomical planes defined for the Reference Mannequins.	26
2.11	World Coordinate System definition, registration process, and definition of pivot point (origin) of WCS. (a) Orthogonal views. (b) Isometric view.	26
2.12	Minimization of the variation between orientations of corresponding ellipsoids with re-labeling and direction inversion . Yellow ellipsoids, 13.a Rectus Abdominalis from Tall Chubby (reference $[\mathbf{u}_c, \mathbf{v}_c, \mathbf{w}_c]$) and Tall Slim (modified orientation $[\mathbf{u}, \mathbf{v}, \mathbf{w}]$). (a) Incorrect status for axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$. (b) Re-labeled axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$ in (a) . Correct labeling, incorrect direction for axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$. (c) Direction inversion of axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$ in (b) . Correct status for axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$	27
2.13	Correction of lateral ellipsoid symmetry of ellipsoids from Tall Chubby with only legs displayed for the example. (a) Asymmetric model. (b) Symmetric model.	28

2.14	Correction of central ellipsoid symmetry of ellipsoids from Tall Chubby. (a) Asymmetric model. (b) Symmetric model.	28
2.15	Tailor measuring of ellipsoid mannequins with heights at which $m_T()$ is applied and example of cross sections obtained and measured with $m_T()$ of breast and hips of Small Slim ellipsoid model. (a) Heights at which 2D convex hulls are computed. (b) Examples of 2D convex hulls.	29
2.16	Body subsets of ellipsoids for segmented interpolation scheme. Each subset is interpolated with different subsets of the input measurements Me . (a) Measurement dependency for body neighborhoods (subsets of ellipsoids). (b) Example of subsets of ellipsoids influenced by different measurements.	31
2.17	Example of synthesized lower body neighborhoods using segmented interpolation scheme. Synthesized mannequins are transparent. Reference Mannequins (RM) are marked with RM_i . RM_1 : Small Chubby. RM_2 : Tall Chubby. RM_3 : Small Slim. RM_4 : Tall Slim.	32
2.18	Examples of synthesized ellipsoid-based mannequins using segmented interpolation approach.	34
2.19	Cushion-based mannequins. These mannequins correspond to the same mannequins in Figure 2.18 with ellipsoids converted to cushions.	34
2.20	Visual comparison of Mesh-based Model vs. Cushion-based Mannequin synthesized using the measurements from the Mesh-based Model. (a) Mesh-based Model. (b) Cushion-based Mannequin.	35
2.21	Interaction simulation of Slim Tall model and garment using cushion model and showing rigid-body vs. soft-body interaction. Visualization: Constructed by us in Three.js [41]. Simulation: Constructed by us in Ammo.js [5]. (a) Solid-color garment. (b) Wireframe garment.	36
2.22	Interaction simulation of Chubby Small model and scaled garment using cushion model and showing rigid-body vs. soft-body interaction. Visualization: Constructed by us in Three.js [41]. Simulation: Constructed by us in Ammo.js [5]. (a) Scaled garment. (b) Wireframe scaled garment.	37
2.23	Smooth representations of the Cushion-based Mannequins. These representations <i>are not</i> the aim of the present manuscript, rather for future ones.	38

List of Tables

1.1	Manuscript related to this Master's Thesis.	2
1.2	Co-authors of this Thesis' Article.	2
1.3	Awards and Recognitions obtained by the Student related to this Master Thesis . . .	3
1.4	Informatics and industrial abilities	3
1.5	Relevant Courses	4
2.1	Comparison of previous approaches found in the literature plus our contribution. . .	13
2.2	Characteristics of the input data of the reference 3D model.	19
2.3	Tailor measurements Me in cm for the Reference Mannequins RM , $Me_i \in RM$. . .	23
2.4	Relative error between input and real measurements in set of synthesized mannequins. Measurements performed with m_T	33
2.5	Tailor measurements of mannequins shown in Figures 2.18 and 2.19. Measurements in cm.	33
2.6	Relative error between Mesh-based Model and Cushion-based Mannequin measurements (cm). Measurements performed with m_T	35

1

Introduction

Digital modeling of human representations or mannequins is a topic with an ever-increasing interest in the research and industrial communities. The possibility to obtain a 3D model approximation of any human in a cost-effective manner presents benefits for applications such as virtual tailoring, garment fitting simulation, human motion modeling, avatar creation, character design, etc. Therefore, special interest is placed on finding methods to obtain such mannequins with minimal information and human interaction.

This work presents a published journal article that contributes to the problem stated in this introduction. Sections 1.1 and 1.2 details the article presented in this thesis and lists all the co-authors associated to the manuscript. Section 1.3 summarizes the industrial and academic research projects associated with the Master Thesis. Section 1.4 reports the distinctions of the student during his Master Thesis. Finally, Section 1.6 explains to the reader how to follow this document.

1.1 Summary of the Manuscript

The published article, with its respective authorship and bibliographic information, is listed in Table 1.1.

Table 1.1: Manuscript related to this Master’s Thesis.

Item	Bibliographic Information	Type / Status
1	Samuel Velez-Sanin, Juan Gutierrez, Jorge Correa, Carolina Builes-Roldan and Oscar Ruiz-Salguero. Applied Sciences, p-ISSN: 2076-3417, volume 12, issue 19, Publisher MDPI. url= https://www.mdpi.com/2076-3417/12/19/9742 , DOI: https://doi.org/10.3390/app12199742 , Received: 10 May 2022; Published: 28 September 2022. Indexed in Scopus (Q2), Scimago (Q3), Publindex (A1).	Journal Article / Published.

1.2 List of Co-authors of the Journal Article

The names and affiliations of the co-authors of the article presented in this thesis are listed in Table 1.2.

Table 1.2: Co-authors of this Thesis’ Article.

Name	Affiliation
Dr. Eng. Jorge Eduardo Correa Panesso	Manufactura Cohesiva S.A.S., Medellín, Colombia
M.A. Carolina Builes-Roldan	Laboratory of CAD CAM CAE, Universidad EAFIT, Colombia
Eng. Juan Gutierrez	Manufactura Cohesiva S.A.S., Universidad EAFIT, Colombia
Eng. Samuel Vélez-Sanin	Laboratory of CAD CAM CAE, Universidad EAFIT, Colombia
Prof. Dr. Eng. Oscar Ruiz Salguero	Laboratory of CAD CAM CAE, Universidad EAFIT, Colombia

1.3 Projects

The student executed the previously cited research in the context of industrial projects hosted by Manufactura Cohesiva S.A.S. The student was granted a 24-month research internship at Cohesiva in the context of the collaboration agreement between Manufactura Cohesiva and Universidad EAFIT for Master and PhD students. The student participated in the following projects:

1. **Project: TEXTILE VIEWER 2020-2021:** development of a web 3D environment for the visualization and simulation of virtual garment fitting over digital mannequins. *Institutions:* Manufactura Cohesiva, Colombia; Laboratory of CAD CAM CAE, Universidad EAFIT, Colombia.
2. **Boundary Element Method:** implementation of the source-node displacement method for the solution of singularities in the equations that tackle the boundary element problem in the

field of Fluid Dynamics. *Institutions:* Laboratory of CAD CAM CAE, Universidad EAFIT, Colombia.

1.4 Distinctions

The following table presents the distinctions and acknowledgments that the student and the Master Thesis team achieved during the post-graduate process:

Table 1.3: Awards and Recognitions obtained by the Student related to this Master Thesis

Distinction	Context	Observation
Post-Graduate Scholarship: Recognition for the best academic performance (GPA) of the graduating students of the Engineering School in 2020-1	Universidad EAFIT (2020-2 to 2022-2)	37,592,570 COP covering academic credits of Master Courses (not including homologated undergraduate emphasis line courses)

1.5 Academic Impact

The industrial and informatics abilities acquired as a result of the work performed both in the master's degree and the industrial internship are listed in Table 1.4.

Table 1.4: Informatics and industrial abilities

Abilities	Period	Description
Computational geometry for web technologies	August 2020 - December 2022	Development of computer graphics technologies applied in the web and cloud computing industry.
Micro-services and virtual machines protocols	November 2020 - February 2021	Design, creation, and deployment of micro-services through HTTP and HTTPS protocol.
Data structures and algorithms	November 2020 - June 2022	Necessary for all projects
Computational simulations	November 2020 - November 2022	Manipulation of Position-based Dynamics engines for the simulation of human-cloth interactions.

Table 1.5 presents the courses that provided the student with the necessary tools and knowledge to conduct the research project.

Table 1.5: Relevant Courses

Course	Semester
IM0242 Introduction to CAD CAM Systems*	2017-1
IC0717 Introduction to the Finite Elements Method	2019-2
IC0896 Mechanics of Advanced Continuous Media	2019-2
IC0916 Introduction to the Boundary Element Method	2020-1
IC0920 Advanced Mathematics for Engineers	2020-1
IM0603 Geometric Modeling	2020-2
EI0813 Academic Writing and Research Skills	2020-2
IM0912 Numerical Solution of Differential Equations	2020-2
IM0911 Programming in Engineering	2021-1
ST0914 Data Structures and Algorithms	2021-2

*Although the IM0242 course was completed during the undergraduate studies of the student, it established the basis in computational geometry, programming and computer science for his master's degree and the industrial internship.

1.6 How to Read this Document

This document presents the developments of a research executed at the Laboratory of CAD CAM CAE at Universidad EAFIT (Colombia), in conjunction with Manufactura Cohesiva S.A.S. The results are a combination of data structures and algorithms, computational geometry, mathematics, numerical methods, and numerical simulations. **The article included in this thesis has been published by a peer-reviewed journal.**

Chapter 2 presents the published Journal Article. This chapter proposes a methodology to parametrically model 3D digital representations of female human bodies. The devised method consists of (1) the approximation of a template/example digital mesh with ellipsoids, (2) the construction of a set of five reference models with different measurements based on the ellipsoids approximation, and (3) the creation of a set of functions that synthesizes a new mannequin (set of ellipsoids) given a set of desired tailor measurements.

Finally, relevant conclusions of this work as well as possible future improvements on this research are presented in Chapter 3.

2

Measurement-driven Synthesis of Female Digital Mannequin using Convex Sub-volumes

Samuel Velez-Sanin^{1,2}, Juan Gutierrez^{1,2}, Jorge Correa², Carolina Builes-Roldan¹ and Oscar Ruiz-Salguero¹

¹ Laboratory of CAD CAM CAE, Universidad EAFIT, Cra 49 no 7-sur-50, Medelln 050022, Colombia

² Manufactura Cohesiva SAS, Cra 32B no 10-30, Medelln 050021, Colombia



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Context

Samuel Velez-Sanin, Juan Gutierrez, Jorge Correa, Carolina Builes-Roldan and Oscar Ruiz-Salguero. Applied Sciences, p-ISSN: 2076-3417, volume 12, issue 19, Publisher MDPI. url= <https://www.mdpi.com/2076-3417/12/19/9742>, DOI: <https://doi.org/10.3390/app12199742>, Received: 10 May 2022; Published:

Abstract

In the context of computer-aided apparel-fitting simulation, the problem of generating (a) simulation-inexpensive and (b) tailor-measurement-driven digital mannequins is central. Three-dimensional scanning of human bodies produces high-fidelity datasets. However, this technique does not satisfy conditions (a) and (b) above. In addition, it requires extensive data cleaning and processing. Existing approaches to this problem broadly fall into these mainstreams: (i) biased scaling, interpolation, or morphing of template models; or (ii) bottom-up construction of anatomy (bone medial axis, kinematic joints, muscles, skin, and other layers). Both alternatives imply extensive scanning, application of heuristics, tuning, and storage, among other tasks. Both alternatives produce non-convex datasets that have to be processed further for cloth-body interaction simulation, as physics engines require some type of data convexity for realistic simulations. This manuscript presents a modeling methodology that partially overcomes these limitations by (1) coarsely approximating a template female body with sets of convex volumes (ellipsoids and *cushions*), (2) building a set of Reference Mannequins for a particular set of extreme and average tailor measurements, and (3) creating sets of functions that synthesize new individuals of digital mannequins as reunions of convex volumes that satisfy specified tailor measurements. These mannequins present a reasonable and realistic demeanor. At the same time, they are shown to be economical at the stage of simulation of garment fitting. Future work is encouraged to define kinematic chains for straightforward pose definition, modeling male bodies, and exploring the behavior of the synthesis functions with more parameters.

Keywords: measurement-driven digital mannequins; human body modeling; parametric modeling; tailor measurements; convex-volume-based modeling

2.1 Introduction

2.1.1 Context

Parametric modeling of the human body (in the relevant literature [1,2]) is the process by which 3D digital representations of diverse body shapes and sizes can be synthesized from input measurements and example models. An advantage of parametric human body modeling is the possibility of economically and flexibly avoiding scanning or manual digital sculpting to obtain 3D models of different phenotypes [1]. Parametric modeling of humans is applied in virtual tailoring, garment fitting simulation, human motion modeling, avatar creation, character design, etc.

Digital mannequin realization and virtual garment trial directly implement physics and mathematical theories and tools (statistics, differential geometry and equations, signal processing, kinematics, multi-particle systems, thin-plate energy, strain modeling, etc.). Time optimization in these fields touches topics such as scalar and vector fields, hash functions, lattice geometry, topology, etc. Garment fitting [3,4] and mannequin modeling [1] rely heavily on computational geometry and topology tools.

Usual parametric modeling produces mappings between body surface point clouds and anthropometric (i.e., tailor) measurements. A goal is to produce new point clouds that obey extended sets

of tailor measurements. Prescribing the position of massive amounts of points by using analytical forms or constraints easily produces unnatural, illegal, self-intersecting, or non-manifold meshes or point clouds. Additional tuning and processing are then required. In point-cloud-based modeling, execution time and storage expenses are very large.

2.1.2 Research Strategy and Scope

This manuscript applies to digital model synthesis, the well-known practice in the artistic drawing and sketching domain of approximating a human or animal body by a set of ellipsoids. This set of ellipsoidal primitives effectively captures the pose and demeanor of the (static) female model. It does not concern itself with the details. A bijective mapping tailor measurements vs. ellipsoid set is computed. This mapping allows the synthesis of a female mannequin that satisfies a set of tailor measurements. It also allows extraction of the tailor measurements of a given mannequin. We then use a derivative convex primitive, called *cushion* (the convex hull of two ellipsoids), to complement the approximation of the female human body. We do not seek to arrive at a mesh representation of the body. Therefore, our approach does not incur the expenses of mesh cleaning, repairing, convex decomposition, etc. The approximation of the female mannequin by using a set of convex primitives is accepted by some physics engines (e.g., [5]) to simulate garment-body interaction. Notice that we do not, in this manuscript, model garment-body interaction.

Our manuscript does not attempt the automated synthesis of digital mannequins from images, videos, or point clouds (neither static nor dynamic) through feature extractions and scalings, among other procedures. Our manuscript does not address mannequin kinetics or motion, nor recognition/classification of subject actions or activities. For readers interested in these topics, references [6, 7] may provide useful insight. The interest of our effort is to use a convex primitive approximation of a digital mannequin and tailor measurements in order to create other digital individuals with diverse sizes. Our manuscript executes interpolation among sizes of ellipsoid-based mannequins by finding and using bijections between sets of tailor measurements and ellipsoid-based mannequins. Our manuscript addresses static (as opposed to motion) scenarios.

Our industrial sponsor has female mannequins and garments as its priority. This fact explains why this publication does not address male digital mannequins. Future efforts will do so.

The problem that this manuscript addresses is formulated as:

Given

1. Me : A set of measurements $Me = [He, Sh, Br, Wa, Hi]$ that describe the shape of a female body. With He : Height, Sh : Shoulder width, Br : Breast perimeter, Wa : Waist perimeter, and Hi : Hip perimeter.

Goal

1. B : 3D mannequin approximation of a female body that satisfies a particular set of tailor measurements Me . B is a set of convex volumes.

2.1.3 Manuscript Structure

This manuscript is structured as follows: Section 2.2 reviews the existing literature, drawing conclusions to justify the manuscript. Section 2.3 explains the methodology followed to model and

synthesize the mannequins. Section 2.4 presents the results of our method and a particular application to demonstrate its usefulness. Section 2.5 concludes the manuscript and discusses relevant future endeavors.

2.2 Literature Review

The current literature for parametric modeling can be divided into two main categories: (i) non-convex example-based modeling through scalings and morphings, and (ii) bottom-up construction of anatomy-based models (bone medial axis, joints, muscles, and skin). This section seeks to give a taxonomy and summary of the current methods found in the literature, as well as to expand on the different approaches found for both categories.

2.2.1 Non-Convex Example-Based Modeling

The most common approach found in the literature for the parametric modeling of human bodies is non-convex example-based modeling. For this general approach, researchers mainly extract *features* (e.g., cross sections, anatomical landmarks, and patches) from 3D-scanned point-clouds, digital template models, or images. Afterwards, they determine the relation between measurements and features in order to either deform a template model or interpolate multiple examples.

In general, these approaches present the following limitations: (1) The synthesized model is a non-convex mesh or point-cloud. (2) The resulting model needs further processing to be used for simulations concerning collision detection. (3) They require the use of expensive algorithms for feature extraction, deformation, ensuring surface continuity, and surface-fitting. (4) Re-computation/deformation of non-convex surfaces is needed in order to define new poses. (5) This method is dependent on hardware and/or a large database of examples. A summary of the different approaches found for this particular category is presented next, where each particular reference is discussed in further detail.

Deformation of a Single Template/Example Model

References [8–16] extract *features* from a single digital template model or 3D scan and apply deformation functions in order to synthesize variations that satisfy input measurements.

- Reference [8] imposes symmetric constraints to the ‘SCAPE’ parametric model. These symmetric constraints are defined as symmetry-related matrices and are applied during pose and shape deformation to provide a resulting symmetric model.
- Reference [9] proposes a tensor decomposition technique to model human bodies based on data (shape and pose) of multiple subjects. They use such data to train a deformation method that considers pose and shape parameters in conjunction rather than independently. This method is applied to a template model.
- Reference [10] proposes the segmentation of a template model (point-cloud) into regular intervals. These intervals are subsets of point-clouds to which shape control lines (SCL) are fitted. The SCLs are then modified by applying centroid-based and ratio-based scalings to produce variations of the template.

- Reference [11] extracts contour (*features*) from a scanned model. These contours are measured and translated vertically according to the template model’s height and the input height. The shape of the scanned model is then modified by applying linear anthropometric rules to produce an adaptive mannequin.
- Reference [12] extracts shape and measurement information from a template model. The authors identify key parameters that define the scaling for the global deformation (responsible for general shape) and feature factors for local deformation (of specific parts of the body). Nonlinear interpolation is used to deform the overall shape and critical parts of the template model based on the key parameters.
- Reference [14] extracts cross sections from a scanned dataset of a physical mannequin. The initial locations of the cross sections are obtained using statistical anthropometric data. These cross sections are deformed by resizing and relocating according to input anthropometric data (measurements) that describes the desired geometry.
- Reference [15] extracts cross sections and characteristic points (*features*) from a template model. Then, characteristic sizes are calculated (heights and circumferences) based on the features. Nineteen main control points are established and used to perform a three-dimensional lengthwise axial deformation. Radial deformation is used to perform girth-wise or area deformations.
- Reference [16] obtains parameter-to-geometry correlations by using radial-basis interpolation over a number of 3D scanned models. These correlations allow for the creation of deformation functions. A template model is then deformed through skeletal deformation, and geometric and energy-based processes are used to calculate vertex displacement.
- Reference [13] performs a manual segmentation of a template model and applies spline and radial-basis deformation functions and continuity filters to change the shape and size of the template model.

Synthesis through Multiple Example Models

References [2,17–25] extract *features* from sets of 3D scans of different individuals and correlate their variations in size and shape to each of their measurements. With such correlation, new individuals can be produced based on input measurements.

- Reference [2] proposes the creation of a database from scanned models. Correlations between the meshes (feature points and curves) and semantic parameters are created and computed as a linear system of equations. The system of equations has its complexity reduced through PCA. New models are produced by modifying input models or finding and modifying similar models (from databases) to satisfy input measurements.
- References [17, 18] preprocess 250 (125 females and 125 males) scanned models from the *SizeKorea* database. The models are categorized, and the correlations between body shape variation and body sizes are extracted through statistical analysis (PCA). With such correlations, new models are obtained through shape parameter optimization techniques and radial-basis function (RBF) deformation of a template surface.

- Reference [19] obtains a set of thousands of scans, for which they extract and correct landmarks. Then, PCA is performed to extract the parameters that define shape variation, which are stored in a database. Moreover, a system in which users can have access to individual 3D scanned data and personalized body-shape modeling is presented.
- Reference [20] presents a unified model that describes pose, shape, and muscular deformation. A set of 550 full-body scans of 114 subjects is obtained, registered, and encoded. Rotation-invariant encoding allows for the creation of semantic regression functions (PCA-based technique). The regression functions are used to generate arbitrary models.
- Reference [21] constructs a database of 160 (80 male and 80 female) body scans. PCA is then performed to parameterize the data and characterize the tendency of shape variation and modeling parameters, and their correlation with anthropometric parameters. Through such correlations and a non-linear error-optimization-based shape modeling method, an arbitrary model can be obtained from user-specified measurements.
- Reference [22] extracts feature points from a set of scanned models. The feature points are used to create feature curves, which are then parameterized. Using a numerical optimization-based scheme, a new model can be synthesized by interpolating certain examples from the database. These examples are selected through an optimization algorithm.
- Reference [23] proposes a learning-based method to define the relationship between feature curves (wireframes) and anthropometric measurements. Such a relationship is built using a deep neural network (DNN) based on a test dataset and used to build new wireframes. New meshes can be created by interpolating the new wireframes into patches.
- Reference [24] proposes a modeling scheme called SMPL, which uses 2100 female models from the CAESAR project database to train a set of parameters. Such parameters are used in linear blending functions (i.e., shape, skinning, and pose) and a regressor to reconstruct a new mesh from the vertex of a template mesh.
- Reference [25] proposes the extraction of measurements from 1024 bodies using VR controllers (i.e., HTC Vive). These measurements are then related to the SIMPL [24] model shape parameters. With such relations, the author train four regressors that allow the creation of new meshes from body measurements obtained with the VR controllers.

Feature Extraction from Photographs

References [26–32] use photographs to extract silhouettes (*features*) and feature points that are used as references to deform and fit a template model, or to reconstruct a new model from the extracted features.

- Reference [26] captures orthogonal pictures of a person and extracts silhouettes. Feature points are obtained from the silhouettes and used to define a linear affine mapping of the correlation between the template model and the silhouettes. This mapping is then used to define and apply shape deformation to the 3D template model.
- Reference [27] manually defines feature points on three orthogonal pictures of a person. From the feature points, a silhouette is extracted and a skeleton is automatically fitted by applying

affine transformations and Barycentric interpolation. A template model’s skin (surface) is then deformed through piecewise affine transformations and 2D-to-3D mapping with the skeleton and silhouette information.

- Reference [28] applies a segmentation method on two orthogonal photographs of a subject to extract contours (silhouettes). The silhouettes are correlated to silhouettes of a template model, and feature points are extracted using morphology rules and template-based feature extraction algorithms. The authors use the model and silhouette photographs to perform view-dependent deformation of the template model.
- Reference [29] presents a modeling scheme in which the authors deform a template model to best fit the user’s shape. The first step consists of fitting the template to a user-generated point-cloud via 3D scans and feature-point extraction. The second uses low-resolution 2D images to estimate the shape and pose of the human body, assisted by boundary constraints.
- Reference [30] presents a method for rebuilding 3D models based on a set of seven template models and orthographic images of a subject. The method consists of extracting contours from the images and scaling contours from the template models according to the extracted contours.
- Reference [31] estimates the 3D shape and pose of a subject from a single image. This process consists of regressing the 3D positions of the vertices of a SMPL-template mesh via graph convolutional networks, avoiding the use of anthropometric parameters.
- Reference [32] propose the reconstruction of 3D meshes from a single image. A graph convolutional network (GCN) is used to directly predict the 3D locations of mesh vertices from the input image. Anthropometric parameters are integrated into the GCN to improve the reconstruction accuracy.

2.2.2 Anatomy-Based Modeling

A particular family of approaches found in the literature consists of bottom-up manual modeling of individuals. These approaches focus on the influence of the pose over muscle deformation and its influence on the shape of the model (skin). They propose building a kinematic skeleton to which muscles and tissues are modeled and attached. Then, the shape of the muscles and tissues is parameterized as a function of the state of the kinematic joints. Finally, a surface-fitting procedure is performed to reproduce skin over the deformed muscles. These approaches present the following principal disadvantages: (1) A non-convex model is produced; (2) High computation expenses due to deformation algorithms and surface fitting with each change of state in the kinematic joints; (3) Modeling of multiple internal elements to reproduce external surfaces; (4) No possibility to synthesize different phenotypes from input measurements.

Reference [33] utilizes isotonic contraction and tension parameters to formulate muscle deformation. No skin approximation is presented. Reference [34] presents a scheme to approximate muscles as deformed cylinders that are parameterized to change size and shape with changes in joints. Skin is presented as an elastic surface that is deformed with changes in size and shape of the underlying components (tissue and muscle).

2.2.3 Conclusions of Literature Review

The main conclusions of the literature review are presented in this section with a summary exhibited in Table 2.1. This table exhibits a comparison between the advantages/disadvantages of previous schemes and of the approach presented in this manuscript. Such a comparison seeks to support the contributions made by the proposed approach.

Table 2.1: Comparison of previous approaches found in the literature plus our contribution.

Approach		Refs.	Advantages	Disadvantages
Non-Convex based Synthesis	Example-based Approach	[2, 8–16, 18–32, 35, 36]	(1) Models with intricate details can be reproduced. (2) Continuity of mesh surface is achieved. (3) Anatomic fidelity of the model.	(1) A non-convex model is produced. (2) Needs further processing steps to generate a ready-to-simulate model. (3) Expensive algorithms for deformation and surface-fitting. (4) Pose limitation or need to recompute/deform surfaces for pose changes. (5) Dependent on hardware and/or a large database of examples.
Non-Convex Based Approach:	Anatomy Bone, Muscle, Tissue Construction	[33, 34]	(1) Anatomic fidelity of the model. (2) High kinematic fidelity can be achieved.	(1) A non-convex model is produced. (2) High computation expenses. (3) Construction of unnecessary internal elements to reproduce external surfaces. (4) Phenotype limitation.
Synthesis Based on Convex Volumes		Our approach	(1) Low computational costs. (2) No intermediate steps for the preparation of the model for physics simulation. (3) Simple and straightforward parameterization with minimal tuning. (4) Reduced storage of data. (5) No need of re-computations of surfaces for pose changing.	(1) Low model resolution, leaving out intricate details of the body. (2) Model surface does not have C^1 surface continuity.

In the current literature, the human body is modeled as non-convex meshes, with exceptions found in some components of the models produced by anatomy-based methods. These non-convex meshes are computationally expensive to process for pose variation and collision detection simulations (e.g., garment-fitting), among other implementations. In addition, example-based approaches present particular disadvantages in (1) requiring expensive hardware, (2) storage of large amounts of

data, (3) usage of smoothing and surface-fitting algorithms, and (4) expensive extraction of features and identification of feature–parameter relations. It is also noted that anatomy-based approaches do not parameterize the general shape and size of the model. In contrast, they require manual intervention for modeling a particular phenotype.

To overcome these limitations, this manuscript proposes a parametric modeling scheme based on convex volumes. The scheme synthesizes sets of convex volumes (mannequins) from sets of tailor measurements and a small set of manually created Reference Mannequins (RM). Furthermore, the synthesized models satisfy the input measurements. This approach presents the following **contributions**: (a) avoids the need for hardware and the storage of large amounts of data, (b) enables pose variation through kinematic chains without re-computing surfaces, (c) simple and straightforward parameterization with minimal tuning, and (d) the synthesized mannequins are ready-to-simulate and do not need further processing. In conclusion, to the best of our knowledge, no other approach based on convex volumes is found in the literature. Hence, our approach proves novel.

2.3 Materials and Methods

The proposed methodology consists of approximating a 3D model with convex volumes (ellipsoids and cushions), which we call a 3D mannequin. This mannequin is parameterized (synthesized as a function of tailor measurements) in order to obtain measurement-driven 3D mannequins. Such mannequins satisfy the desired measurements with a minimum margin of error. The main steps performed to produce the measurement-driven mannequins are as follows (see also Figure 2.1):

1. A reference 3D model is manually approximated/traced with ellipsoids to produce a Base Mannequin (BM). Furthermore, an ellipsoid-to-cushion post-process is presented to improve the convex volume approximation after it has been parameterized. See Section 2.3.2.
2. The BM (set of ellipsoids) is then used to instance a set of Reference Mannequins (RM). Each one of these Reference Mannequins (RM_i) satisfies a particular set of five tailor measurements. See Section 2.3.3.
3. Based on the known data of RM (geometry and measurements), a set of functions $F(Me)$ is created. This set of functions synthesizes the geometry of a measurement-driven mannequin that in return satisfies the given measurements in Me . See Section 2.3.6.
4. Finally, the measurement-driven mannequin can be synthesized by computing $F(Me)$.

Problem Specification

These steps are explained in more detail in the following subsections (see Sections 2.3.2, 2.3.3, and 2.3.6). The problem of finding the parameterization for the 3D mannequins can be specified per the following **given** and **goal**:

Given:

1. A : A set of points in \mathbb{R}^q . Each component j of a point x ($x \in A$), with $j = 1, 2, \dots, q$, represents a measurement of the human body in Me (e.g., height, shoulder width, etc.). The following conditions must be considered:
 - (a) $x_j > 0, \forall j = 1, 2, \dots, q$.

- (b) L : A set of q ordered pairs corresponding to the lower and upper limits of the components j of x . $L : \{l \mid l_{1,2} > 0, l_1 < l_2\}$
- 2. H : A set of sets of ellipsoids in \mathbb{R}^3 . Each set of ellipsoids B , with $B \in H$, approximates the shape and size of a human body described by a point $x \in A$.
 - (a) Each B has the same number m of ellipsoids and the same topology.
 - (b) Each B satisfies the measurements of a specific point $x \in A$.
 - (c) Each ellipsoid of B is defined by a homogeneous $SO(3)$ coordinate system S and a triad D describing the dimensions of its semi-axes.

Goal:

1. m_T : Function $m_T : H \rightarrow A$; m_T obtains the tailor measurements Me of any model $B \in H$.
2. F : A set of functions $F : A \rightarrow H$, $F = m_T^{-1}$. More specifically, $F : x \rightarrow B$, such that m_T applied to $B = F(x)$ produces the measurements in x . F is a set of functions that, given a set of measurements x , synthesizes a model (geometry) B that satisfies x .

From Figure 2.1 it must be taken into consideration that Steps 1 through 3 are performed only once so as to produce F . The set of functions F is then computed each time a new mannequin is synthesized from defined measurements Me . It is also worth noting that the subject approximated by convex volumes in this manuscript is the female body. The same process could be applied to approximate the male body.

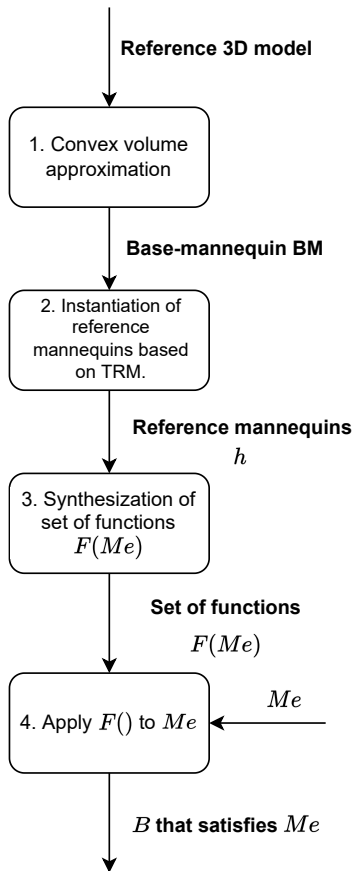


Figure 2.1: Flow diagram of the convex-volume-based measurement-driven approximation. Input: Reference 3D model. Output: Measurement-driven mannequin B . Steps 1 and 2 pre-processing. Steps 3 and 4 are processing.

2.3.1 Rationale for the Mathematical Model

In order to obtain a parametric mannequin, a set of pre-processing and processing steps are carried out. The procedural enumerations and descriptions of these steps are addressed in Sections 2.3.2–2.3.4 for pre-processing and Sections 2.3.5 and 2.3.6 for processing. The current subsection intends to highlight the main mathematical and scientific reasoning that provide support for such steps.

Geometrical and Topological Pre-Processing

Pre-processing seeks to facilitate the bijective mapping ellipsoid set \leftrightarrow tailor measurements by reducing (a) mathematical complexity and (b) numerical instability. Pre-processing (1) manually constructs an ellipsoid set (BM) that approximates a mesh-based model, (2) reduces the degrees of freedom of the ellipsoid set, and (3) lowers the noise level within the ellipsoid set. Pre-processing consists of:

1. Selection of ellipsoids due to their low geometrical complexity, low data-storage, and the benefits of convex volumes present in physics engines;

2. Manual approximation of the 3D reference model by fitting a set of ellipsoids;
3. Symmetrical location of ellipsoids with respect to the sagittal plane;
4. Construction of a set of Reference Mannequins through rigid transformations of the set of ellipsoids;
5. Compliance of Reference Mannequins to sets of tailor measurements;
6. Data processing is performed over the set of Reference Mannequins in order to achieve:
 - (a) Enforcement of symmetry with respect to the sagittal plane;
 - (b) Enforcement of right-handedness in the ellipsoid coordinate systems;
 - (c) Congruence of the coordinate system (definition of World Coordinate System);
 - (d) Re-labeling of SO(3) coordinate systems (i.e., ellipsoid axes) to ensure minimal variation of the interpolation functions in set F .

By definition, our approach seeks large-scale (ellipsoid approximation) geometrical information of the mannequin. This scope filters out small details and noise. In this particular manuscript, such filtering was manually executed by fitting the ellipsoid set to the Base Mannequin. For this process to be executed in a semi-automated or automated manner, we suggest these topics: (a) alpha shape fitting [37] and (b) signal denoising [38].

Processing; Bijective Mapping; Tailor Measurements \leftrightarrow Ellipsoid Sets

Many possible sets of ellipsoids could satisfy the measurements of a particular $x \in A$, generating infinite m_T^{-1} . Therefore, a particular $F \subset m_T^{-1}$ has been selected, such that each $B = F(x)$ satisfies the measurements of an arbitrary x . F is then considered as the set of parametric functions that synthesizes a particular mannequin B given a desired set of measurements x and a set of known tuples of RM (set of Reference Mannequins) containing geometry and measurements.

In addition to the previous precision made about the mapping from $x \rightarrow B$, a set of reasonings is presented for the processing steps (interpolation method). These reasonings seek to avoid instability (erroneous sizing and unnatural demeanor) of the synthesized mannequins (see Section 2.3.6).

1. Selection of a multivariate weighted average (interpolation) method for the definition of F ;
2. Selection of inverse distance weighting (IDW) as the interpolation method due to its minimal tuning and boundary condition characteristics;
3. Limitation of the dimension of the measurement space to reduce the complexity of the interpolation scheme;
4. Segmentation of the interpolation functions dictated by mannequin neighborhoods;
5. Synthesis of neighborhoods by a subset of functions $f_i \in F$ given a subset of measurements (e.g., shoulder width and height);
6. Definition of neighborhoods based on a measurement dependency rationale.

2.3.2 Creation of the Convex Volume Approximation

The basis for all measurement-driven mannequins is composition by a number of ellipsoids that are selectively placed, scaled, and oriented over a reference 3D model. This basis is called the Base Mannequin (BM) and coarsely approximates the shape of a female body given by a reference 3D model. Each other mannequin in this manuscript preserves the same topology of BM , but differs in geometry (i.e., dimensions, position, and orientation of ellipsoids). It should be noted that BM is conformed both by topological and geometrical information, with the latter being the complement of the former and defined as follows:

1. Topology: Set of ellipsoids and rules that define the composition of the 3D mannequin;
 - (a) The mannequin is conformed by a collection of convex volumes (ellipsoids), without boolean union among them;
 - (b) The collection has a finite number of ellipsoids;
 - (c) Each ellipsoid (singleton or pairs) approximates a particular part or area of the body;
 - (d) Pairs of ellipsoids correspond to parts of the body with reflection (symmetry) along the sagittal plane (i.e., left and right);
 - (e) Singleton ellipsoids are symmetric with respect to the sagittal plane.
2. Geometry: Set of geometric properties S (position and orientation) and D (dimensions) that define each ellipsoid.

Approximation of the 3D Model with Ellipsoids

The process of creating the Base Mannequin starts by defining planar data points (see Figure 2.2) over the 3D model (see Table 2.2 for characteristics of the model). These data points serve as guidelines for the creation of ellipsoids and as future references on which some tailor measurements are performed (see Section 2.3.5).

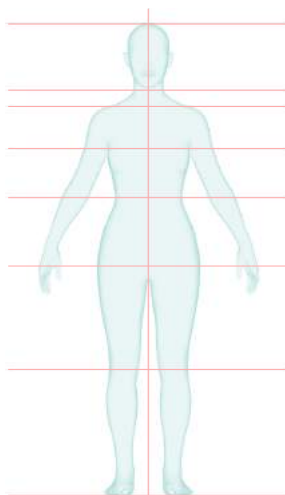


Figure 2.2: Reference 3D model to be approximated by convex volumes. Planar data (red lines).

Table 2.2: Characteristics of the input data of the reference 3D model.

Name	Origin	Number of Faces	Number of Vertex	Borders	Manifold
Reference 3D Model	[39]	4984	4986	0	True

Following the definition of the planar data, a specific region of the body (mainly a principal muscle or area) is selected and traced by creating (placing, orienting, and scaling) one or two ellipsoids as needed (see Figure 2.3b). The intention is to fill up as much space as possible while making sure the ellipsoid(s) is (are) inscribed in the reference 3D model surface (see Figure 2.3). If two ellipsoids are used to approximate a part of the body (see Figure 2.3b), both will serve as the basis of a cushion in a post-processing step.

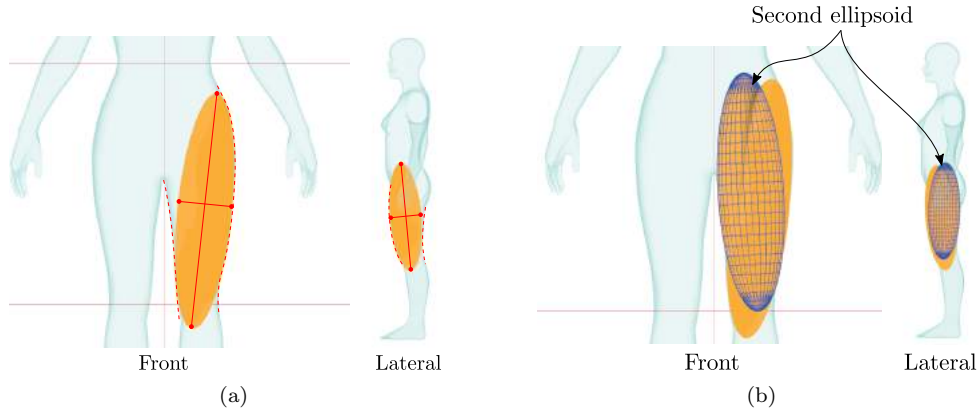


Figure 2.3: Approximation of the left thigh and hip with ellipsoids, front and lateral views. Red dotted line: surface boundary to approximate. (a) Approximation with one ellipsoid. (b) Improvement of the approximation with a second ellipsoid.

The process exhibited in Figure 2.3 is replicated for other parts of the body, excluding the right arm, breast, and leg (see Figure 2.4a). The missing parts on the right hemisphere are obtained by mirroring the analogous ellipsoids of the left hemisphere through the sagittal plane (see Figure 2.4). This preserves proportions and body symmetry. The mirroring process is performed in such way that the $SO(3)$ RHCCS property of each ellipsoid is maintained. It should be noted that symmetry is only obtained in this step of the research. Once kinematics are introduced to the model in future research, symmetry is lost. Take into consideration also that for this step, the shape alone is considered and the measurements of the Base Mannequin are irrelevant.

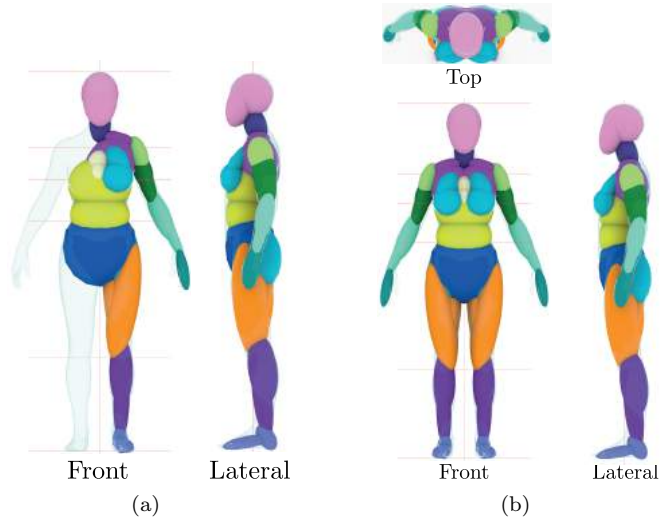


Figure 2.4: Approximation of the reference 3D model with ellipsoids with resulting Base Mannequin (BM) and ellipsoid mannequin and no cushions computed. **(a)** Half of the body approximated. **(b)** The full body approximated and mirroring executed.

Creation of Cushions

As stated previously, some parts of the 3D model are approximated by pairs of ellipsoids (see Figure 2.5). Hence, some regions of the BM , and thus the 3D mannequins, may present gaps or voids between the ellipsoids. Therefore, the pairs of ellipsoids are converted to cushions following an ellipsoid-to-cushion map (see Figure 2.5) in order to obtain a more organic mannequin.

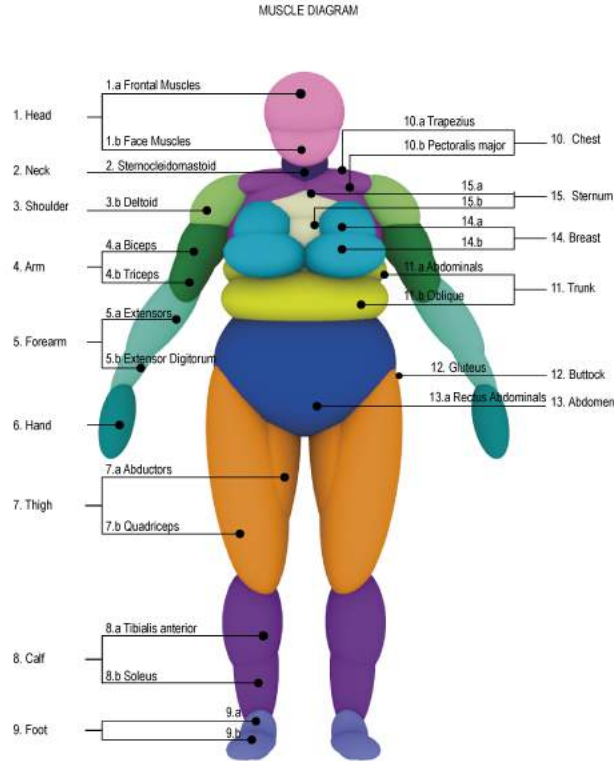


Figure 2.5: Map used to convert ellipsoids into cushions, topology map and ellipsoid model. Pairs of ellipsoids with same color form a cushion.

It is worth noting that the instancing of Reference Mannequins (Section 2.3.3) and the parameterization scheme (Section 2.4.1) is performed over mannequins composed only of ellipsoids. The ellipsoids are the basis of convex volume approximation due to their simplicity. The cushion-based mannequins are a result of post-processing applied to the ellipsoid-based mannequins to partially improve surface continuity and reduce the number of elements. The resulting cushion-based mannequins are intended to be used in different applications (see Section 2.4.3 for an example).

It must be highlighted from Figure 2.5 that pairs of ellipsoids from the same half-space of the sagittal plane and with the same prefix number form a cushion (e.g., 1.a Frontal Muscles and 1.b Face Muscles). Take into account also that the names given to ellipsoids and cushions serve only as a naming convention. There is no absolute anatomical fidelity and our approach does not hold any similarity to the anatomy-based approach mentioned in Section 2.2. The naming convention follows a simple rule: each cushion and ellipsoid is named after the main part of the body that it approximates.

Cushion $C_{E_1 E_2}$ is formally defined as a data type with the following characteristics:

1. $\{E_1, E_2\}$: Point-clouds of ellipsoids in \mathbb{R}^3 ;

2. S_o : $SO(3)$ coordinate system of cushion $C_{E_1E_2}$, coincides with S_{E_1} , the coordinate system of ellipsoid E_1 ;
3. $C_{E_1E_2}$ is defined as $C_{E_1E_2} = \text{ConvexHull}(E_1 \cup E_2)$.

A graphical example of a cushion between two ellipsoids E_1 and E_2 is presented in Figure 2.6, and a model approximated with cushions can be seen in Figure 2.7.

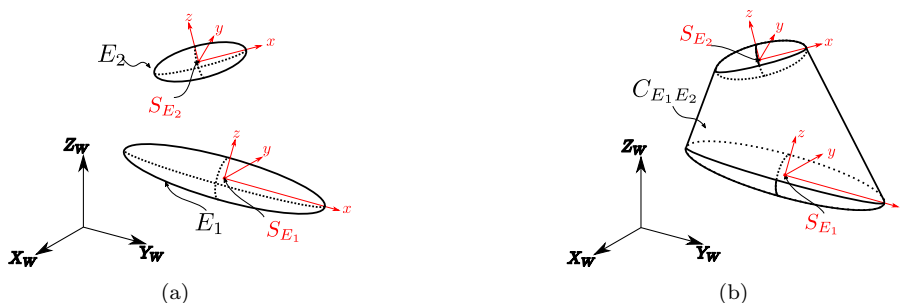


Figure 2.6: Example of cushion $C_{E_1E_2}$, arbitrarily oriented and positioned ellipsoids (E_1 and E_2) in space with convex hull operation between E_1 and E_2 . (a) Ellipsoids E_1 and E_2 . (b) Cushion $C_{E_1E_2}$ between ellipsoids E_1 and E_2 .

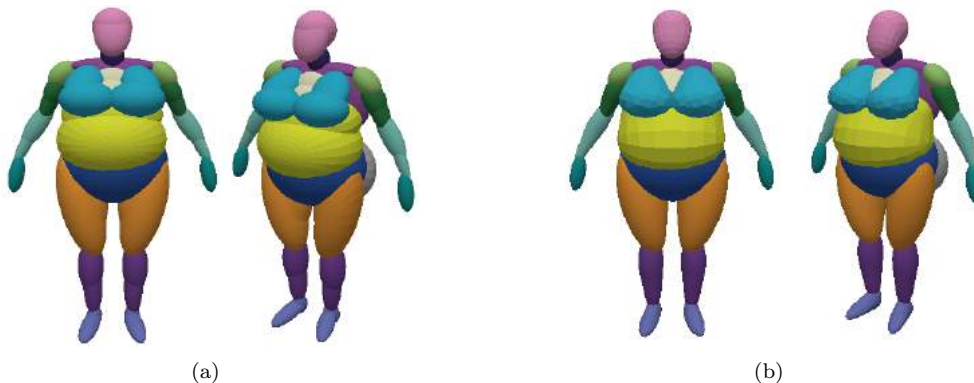


Figure 2.7: Mannequin approximated with cushions and ellipsoids. Ellipsoid mannequin (a) for comparison. Cushions computed according to Figure 2.5. Small chubby mannequin (see Section 2.3.3) as (a) Ellipsoid-based Mannequin and (b) Cushion-based Mannequin.

2.3.3 Construction of Reference Mannequins Based on the Base Mannequin

In order to obtain parameterization, a set RM of five Reference Mannequins with **known** geometry and measurements is created. Each one of the mannequins in RM are instances of the BM that preserve topology but differ in geometry. The **geometry** and **measurements** of each mannequin

in RM are the **parameters** of the set of functions F (see Equation (2.1)) that synthesizes the measurement-driven (parameterized) mannequins. Each RM_i satisfies a different set of five tailor measurements $x \in A$ presented in Table 2.3. The measurements that define each of the models are intended to provide both extreme and average reference geometries and measurements for the interpolation process.

Table 2.3: Tailor measurements Me in cm for the Reference Mannequins RM , $Me_i \in RM$.

Measurement/Model	Small Slim	Tall Slim	Small Chubby	Tall Chubby	Average
Height (He)	148	171	148	171	159
Shoulder Width (Sh)	31	30	45	53	43
Breast Perimeter (Br)	85	84	147	153	117
Waist Perimeter (Wa)	63	63	142	142	104
Hip Perimeter (Hi)	83	84	152	150	117

Creation of the Reference Mannequin Geometries

The process for creating the geometry of each Reference Mannequin $RM_i \in RM$ consists of instancing BM and modifying its geometry. The position, orientation, and size (principal semi-axes dimensions) of each ellipsoid in RM_i is modified such that the measurements in Table 2.3. The step-by-step process performed for every mannequin is presented next (see also Figure 2.8), and the mannequins resulting from this process can be seen in Figure 2.9.

1. The Base Mannequin (see Figure 2.4b) is scaled in the vertical direction to comply with the specific height $He \in x_i$ (see Table 2.3).
2. Each ellipsoid is then manually modified (scaled, rotated, and translated) to obtain a mannequin that visually approximates the tailor measurements $x_i \in A$.
3. Function $m_T(h_i)$ is applied to obtain the current measurements (x_t) of the mannequin. See Section 2.3.5.
4. If some cross section does not satisfy the desired measurement x_i , the ellipsoids that influence it are manually modified (scaled, translated, and rotated) again.
5. Steps 3 and 4 are repeated until the the measurements in Table 2.3 are satisfied.

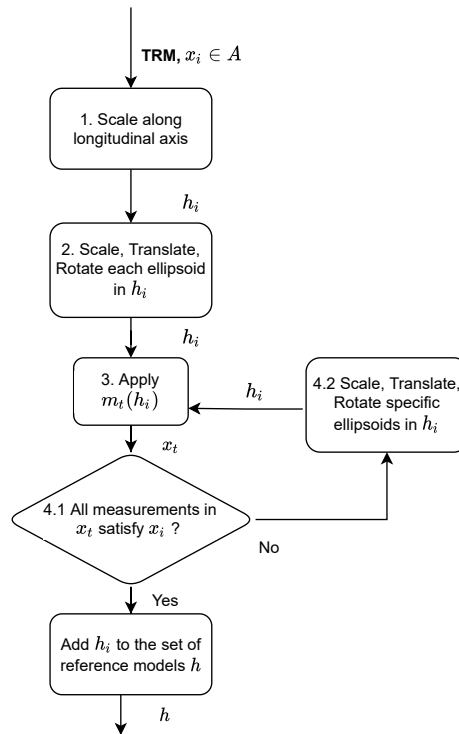


Figure 2.8: Flow diagram for the construction of RM based on BM . Process for a single $RM_i \in RM$.



Figure 2.9: Set RM of Reference Mannequins as ellipsoid mannequins (no cushions) of extreme and average models. From left to right: Small Chubby, Small Slim, Average, Tall Slim, and Tall Chubby.

2.3.4 Cleaning of Reference Mannequin Geometries

Since the Reference Mannequins RM constructed in Section 2.3.3 are manually built, the reference coordinate system on which each model is created may be different. In addition, the models may

not be symmetric with respect to sagittal plane, and the orientations (local coordinate system) of **corresponding ellipsoids** may possess high morphing. Consider “corresponding ellipsoids” as the ellipsoids that are the same topological entity (e.g., 13.a Rectus Abdominalis) and belong to different mannequins from RM . All of the mentioned factors, if not corrected, will lead to an erroneous creation of F and, as a consequence, to the incorrect synthesis of mannequins. Hence, the geometric data of all mannequins in RM are sequentially processed and corrected to ensure consistency in the set. The process for correcting the geometric data is as follows:

1. A common $SO(3)$ coordinate system (WCS) is defined;
2. The position of each model is corrected according to WCS to ensure common placement;
3. The orientations of the sets of corresponding ellipsoids are corrected to ensure minimum variation between analogous axes;
4. The ellipsoids in the right hemisphere are omitted and replaced by reflections (with respect to the sagittal plane) of the ellipsoids in the left hemisphere to obtain symmetry;
5. Central ellipsoids are corrected in order to possess symmetry with respect to themselves along the sagittal plane.

Correction of Mannequins Position

A registration process is performed to define a common placement for the Reference Mannequins. This process consists of defining a set of landmarks and a common coordinate system (WCS), and placing the Reference Mannequins in the same position with respect to the WCS. These landmarks are based on **anatomical planes** (see Figure 2.10) that are widely used in medical fields. Such anatomical planes represent an infinite set of planes perpendicular to the axis in which they are defined:

1. **Coronal plane:** Perpendicular to the ground. Separates front from back.
2. **Transverse plane:** Parallel to the ground. Separates head from feet.
3. **Sagittal plane:** Perpendicular to the ground. Separates left from right.

Now that the directions of the axes \vec{X} , \vec{Y} , \vec{Z} of WCS are given by the normals of the coronal, sagittal, and transverse planes, respectively, the origin (position) of WCS is defined. Such an origin is defined for each Reference Mannequin as follows [40] (see Figure 2.11):

1. In the \vec{Z} direction, the origin is set in the lowest coordinate of the feet;
2. In the \vec{X} direction, the origin is set in the centroid of the shoulder ellipsoids (10.a Trapezius) from the lateral view;
3. In the \vec{Y} direction, the origin is set in the middle point between shoulders (viewed from the front).

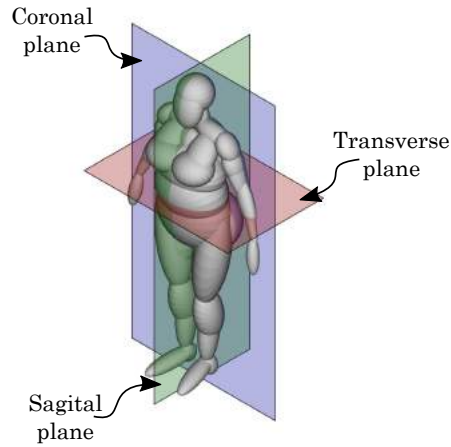


Figure 2.10: Anatomical planes defined for the Reference Mannequins.

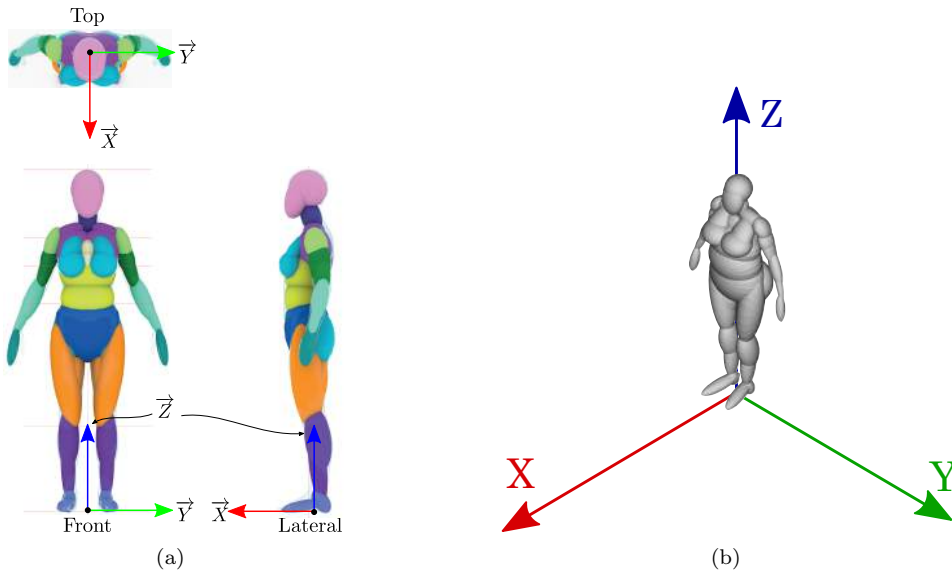


Figure 2.11: World Coordinate System definition, registration process, and definition of pivot point (origin) of WCS. (a) Orthogonal views. (b) Isometric view.

Processing of Ellipsoid Orientation

Now that a common global coordinate system is defined for all mannequins, sets of corresponding ellipsoids should also have a similar coordinate system orientation. Knowing that corresponding ellipsoids differ in geometry (dimensions, position, and orientation), the goal is to obtain smooth morphing or minimal variation (see Figure 2.12) rather than equal orientation. Take, for instance, the example in Figure 2.12a; it shows that analogous axes (e.g., X_1 's) of corresponding ellipsoids

may possess large variation in their orientations. Averaging orientations (applying F) with such morphing (variation) will lead to erroneous results.

In order to make up for the large variation between analogous axes, two processes are performed. Such processes intend to minimize said variation by maximizing the projection between analogous axes by: (1) **relabeling** the orientation axes (e.g., making $\mathbf{u} = \mathbf{v}$ and $\mathbf{v} = \mathbf{u}$), and (2) **inverting** the directions of the newly labeled axes when needed. For the correction of each set of corresponding ellipsoids, one ellipsoid is selected as the reference, and the processes are executed over all the other four corresponding ellipsoids in the set. Note that the dimensions D associated with each axis are considered and also re-labeled accordingly. The orientation axes of each ellipsoid are obtained by performing principal component analysis (PCA) of the point-cloud. The resulting eigenvalues have a \pm sign, which does not allow the definition of a concrete tendency of direction for the eigenvectors (orientation axes). Hence, when **re-labeling** is performed, the resulting axes may possess the maximum projections but with inverted direction (See Figure 2.12b).

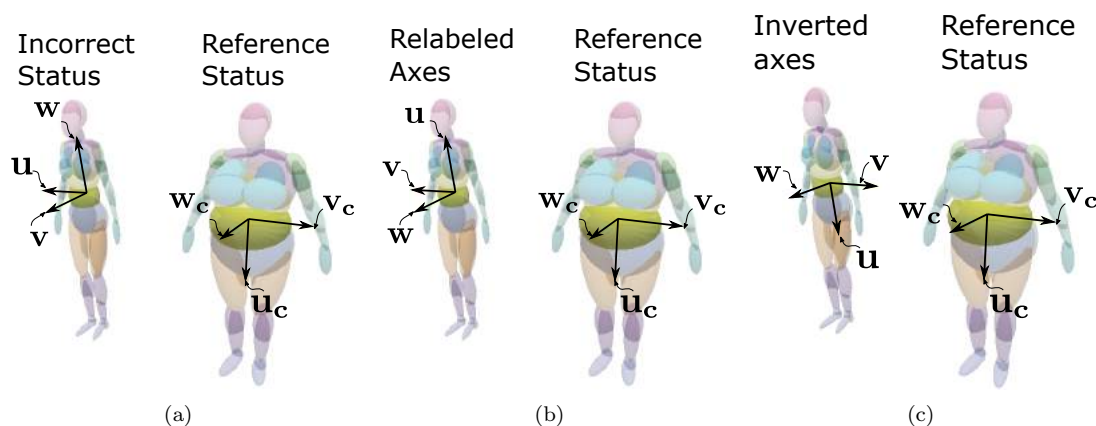


Figure 2.12: Minimization of the variation between orientations of corresponding ellipsoids with **re-labeling** and **direction inversion**. Yellow ellipsoids, 13.a Rectus Abdominalis from Tall Chubby (reference $[\mathbf{u}_c, \mathbf{v}_c, \mathbf{w}_c]$) and Tall Slim (modified orientation $[\mathbf{u}, \mathbf{v}, \mathbf{w}]$). (a) Incorrect status for axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$. (b) **Re-labeled** axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$ in (a). Correct labeling, incorrect direction for axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$. (c) **Direction inversion** of axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$ in (b). Correct status for axes $\mathbf{u}, \mathbf{v}, \mathbf{w}$.

Symmetry Correction

For the symmetry correction, both the central and lateral ellipsoids (ellipsoids with right or left distinction) are considered but approached differently. For instance, the central ellipsoids present asymmetry with respect to themselves through the sagittal plane. In comparison, lateral ellipsoids possess asymmetry in terms of the analogous ellipsoid in the right hemisphere of the sagittal plane possessing a deviation in the orientation, position, and/or dimensions. As a consequence, the following steps are performed in order to fix the asymmetry of the models:

1. For lateral ellipsoids, the right ellipsoids are omitted, and the analogous left ellipsoids are mirrored with respect to the sagittal plane.
2. Due to the mirroring effect, the resulting coordinate systems are left-handed. Hence, the Z-axes have their direction inverted to preserve the $SO(3)$ property. See Figure 2.13.

3. For central ellipsoids, the X-axes are defined orthogonal to the sagittal plane.
4. The Y-axes are projected to the sagittal plane, and the Z-axes are computed as $\vec{Z} = \vec{X} \times \vec{Y}$. See Figure 2.14.



Figure 2.13: Correction of lateral ellipsoid symmetry of ellipsoids from Tall Chubby with only legs displayed for the example. (a) Asymmetric model. (b) Symmetric model.

Note that for Figures 2.12–2.14 some parts of the ellipsoids are rendered in front of others despite really being occluded. Consider this as simply a rendering order issue with transparent objects in the rendering engine.



Figure 2.14: Correction of central ellipsoid symmetry of ellipsoids from Tall Chubby. (a) Asymmetric model. (b) Symmetric model.

2.3.5 Extraction of Tailor Measurements from Models

It is necessary to ensure that all mannequins satisfy the specific set of measurements for which they are created. Thus, a function $m_T(B)$ is defined to simulate tailor measuring over a particular mannequin B ; $m_T(B)$ is used to extract tailor measurements when instantiating the Reference Mannequins (see Figure 2.8), as well as to calculate the relative error of the real measurements x_t vs. the input measurements of the measurement-driven models synthesized with F ; $m_T(B)$ is defined as the following set of steps:

1. Cross sections are obtained at specific heights (see Figure 2.15a) of mannequin B .
2. A 2D (\mathbb{R}^2) convex hull is computed for cross sections corresponding to Br , Wa , and Hi (see Figure 2.15b).
3. The length of the perimeter of each convex hull in \mathbb{R}^2 is calculated.
4. Shoulder width Sh is calculated as the distance between the two outermost points in the Y direction.

The result of applying $m_T(B)$ is a set of measurements x_t that represent the real measurements of B . Please note that Steps 1–3 are performed for Br , Wa , and Hi . For the shoulder width Sh , only Steps 1 and 4 are executed.

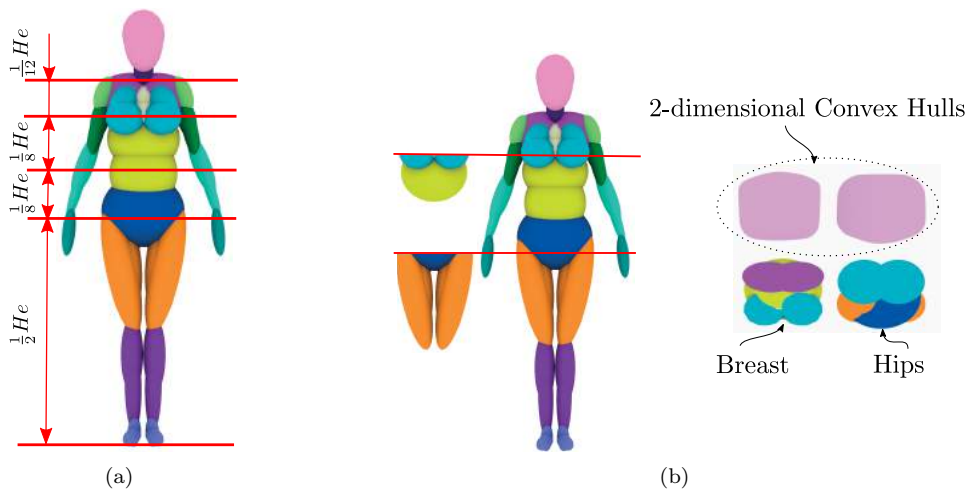


Figure 2.15: Tailor measuring of ellipsoid mannequins with heights at which $m_T()$ is applied and example of cross sections obtained and measured with $m_T()$ of breast and hips of Small Slim ellipsoid model. (a) Heights at which 2D convex hulls are computed. (b) Examples of 2D convex hulls.

It must be clarified that for the purpose of this article, the heights at which the main parts of the body (e.g., belly and breast) are located (see Figure 2.15a) are not considered as a degree of freedom or a variable. These heights are fixed proportions of He . It is known that for each human being, these proportional heights ($\frac{a}{b}He$) might be different. The purpose of this simplification is to reduce the number of degrees of freedom of the model.

2.3.6 Synthesis of Mannequins from Tailor Measurements

Now that a set of Reference Mannequins has been manually (see Section 2.3.3) created and made consistent (see Section 2.3.4), the synthesis of a 3D mannequin B_f (set of convex volumes) from input tailor measurements Me_f can be achieved. Such synthesis is accomplished by computing a set of functions $F(Me_f)$. The synthesized mannequin (B_f) is called a measurement-driven mannequin, and the construction of F corresponds to the parameterization of the convex volume approximation

of the mannequins. The synthesized mannequins are displayed in gray in order to differentiate them from RM and BM .

Parameterization Scheme—Creation of the Set F .

The parameterization scheme consists of building the set of functions $F(Me)$ that synthesizes the geometry (position, orientation, and dimensions of each ellipsoid) of model B_f from input tailor measurements Me_f , such that B_f satisfies Me_f . Each function $f_i \in F(Me)$ synthesizes a geometrical property (S or D) of a particular ellipsoid E_i of B_f . As a consequence, there are $2k$ functions in F , with k the number of ellipsoids in BM . Take into account that each $f_i \in F(Me)$ is an interpolating function (weighted average) with the known tuples (geometry and measurements) of RM as parameters and the input measurements (Me_f) as the variable.

Note that each ellipsoid $E_i \in B_f$ is synthesized by interpolating only the geometrical information (S and D) of its corresponding ellipsoids in RM (see Section 2.3.4 for a definition of corresponding ellipsoids). To understand the definition of the interpolation method, take into consideration the following definitions:

1. RM : set of n Reference Mannequins as a set of tuples $RM = \{(Me_1, B_1), (Me_2, B_2), \dots, (Me_n, B_n)\}$.
2. Me_j : point in \mathbb{R}^5 containing the measurements of the j th Reference Mannequin B_j , $Me_j = [He_j, Sh_j, Br_j, Wa_j, Hi_j]$.
3. B_j : Set of ellipsoids $B_j = \{E_1, E_2, \dots, E_k\}$. $B_j \in RM$, with
 - (a) k : the number of ellipsoids defined in the BM ;
 - (b) $E_i = [D_i, S_i]$: the ellipsoid defined by dimension and coordinate system (position and orientation), respectively.
4. $Me_f = [He, Sh, Br, Wa, Hi]$: measurements of target model B_f describing the shape of the desired female body.
5. B_f : Target model as a set of ellipsoids $B_f = F(Me_f, h)$.

Measurement Dependency.

Considering that each ellipsoid approximates a particular part of the body, it is rational to think that not every ellipsoid in B_f will influence every single measurement in Me_f and vice versa. Thereby, each ellipsoid should not be synthesized as $f(Me_f)$ but as a function of a subset of measurements $me_f \subset Me_f$ that influences it. In other words, each neighborhood of the model (associated subset of ellipsoids) has a unique subset of interpolating functions given by the measurements that influence the specific neighborhood (see Figure 2.16). For example, the measurement Sh has no influence on ellipsoids E from the waist neighborhood (e.g., 11.a_Abdominals). As a consequence, Sh is not an input nor a parameter for the interpolation function f of the waist ellipsoids, but Wa and He are. The construction of specific interpolating functions that depend on subsets of measurements (me) rather than full sets (Me) is called the segmented interpolation scheme.

Interpolation Method

As stated previously, the set of functions F consists of interpolating functions (f). The functions f perform a weighted average of the known geometric data of RM to produce the geometry of a new mannequin B_f . The weights are calculated as a function of the distance between points in space representing the measurements Me_j of each mannequin in RM and the input measurements Me_f .

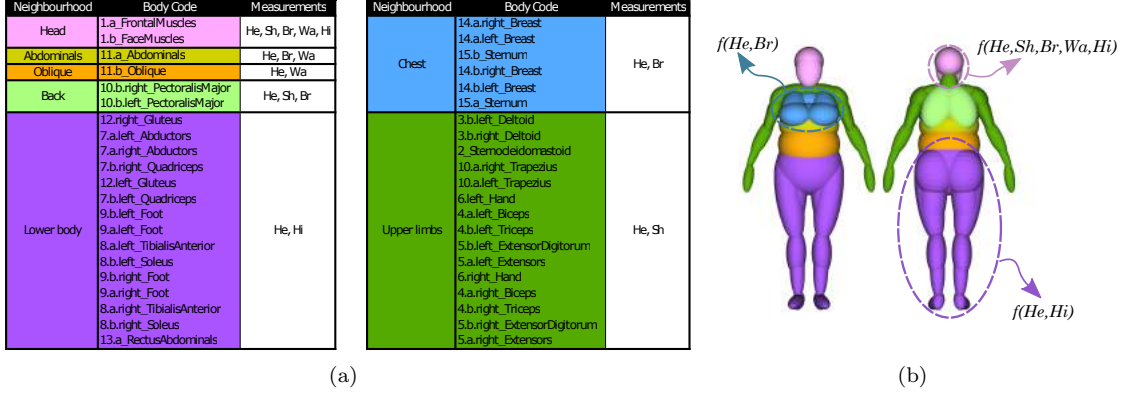


Figure 2.16: Body subsets of ellipsoids for segmented interpolation scheme. Each subset is interpolated with different subsets of the input measurements Me . (a) Measurement dependency for body neighborhoods (subsets of ellipsoids). (b) Example of subsets of ellipsoids influenced by different measurements.

In order to build each $f_i \in F$, radial basis functions and inverse distance weighting (IDW) were tested. The resulting nature of the synthesized mannequins using the former method was unstable due to the need for tuning inherent parameters. The latter rendered the best results with a polynomial degree of 2 (p). Consequently, the IDW method that defines each $f_i \in F$ is expressed in Equation (2.1). Equation (2.1) is presented for a particular ellipsoid E_i and a particular geometrical property (e.g., D or S), following the segmented interpolation scheme. The same process is repeated for other ellipsoids and each geometrical property. Furthermore, consider the following inputs and output for Equation (2.1).

Inputs (variables):

1. me_f : point in \mathbb{R}^l that describes the l measurements of Me_f that influence $E_i \in B_f$, with B_f the synthesized model; $me_f \subset Me_f$.

Inputs (parameters):

1. me_j : point in \mathbb{R}^l that describes the l measurements of Me_j that influence $E_i \in B_j$, with $B_j \in RM$; $me_j \subset Me_j$.
2. Q_j : known geometric property (i.e., D_j or S_j) of $E_i \in B_j$ with $B_j \in RM$
3. $d_j = \|me_j - me_f\|$: euclidean distance between me_f and me_j .
4. p : degree of the interpolation polynomial; $p = 2$.

Output:

1. Q_f : interpolated property (i.e., D_k or S_k) of $E_i \in B_f$; $Q_f = f(me_j, me_f, Q_j)$ with $j = 1, 2, \dots, 5$.

$$Q_f = f(me) = \frac{\sum_{j=1}^n \left(\frac{Q_j}{d_j^p}\right)}{\sum_{j=1}^n \left(\frac{1}{d_j^p}\right)} \quad (2.1)$$

Example of Neighborhood Synthesis

An example of the synthesis of the lower body neighborhood (subset of ellipsoids) is presented in Figure 2.17. This example exhibits the changes of geometric properties (shape) as a function of the dependent measurements (see Figure 2.16a) by following the segmented interpolation scheme.

The synthesized neighborhood is only dependent on measurements He and Hi given that none of the other tailor measurements in Me influence its geometry. Furthermore, note that from Figure 2.17, the geometry of the synthesized neighborhoods (transparent) partially resembles that of the closest Reference Mannequins (RM_i). The mentioned proximity corresponds to the distance in the bidimensional space defined by He and Hi between the points that represents the measurements of the particular synthesized model and of each RM_i . Take into account that the average mannequin in RM is omitted **only** in this particular example for the sake of simplicity.

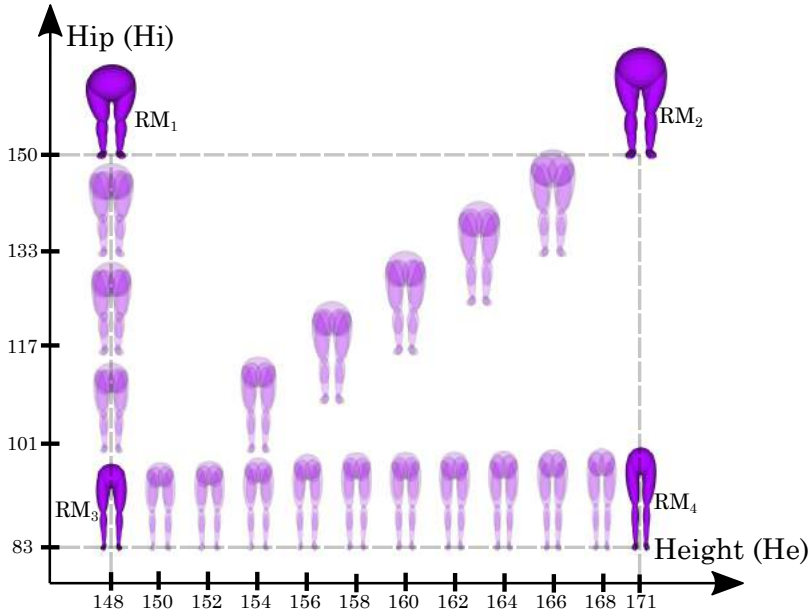


Figure 2.17: Example of synthesized lower body neighborhoods using segmented interpolation scheme. Synthesized mannequins are transparent. Reference Mannequins (RM) are marked with RM_i . RM_1 : Small Chubby. RM_2 : Tall Chubby. RM_3 : Small Slim. RM_4 : Tall Slim.

2.4 Results

2.4.1 Measurement-driven Models Generated via Interpolation

We synthesize a set of 243 measurement-driven mannequins from different sets of input measurements (Me_f). The sets of input measurements are generated by assigning three different values to each of the five tailor measurements that conform Me_f and obtaining all possible combinations ($3^5 = 243$). These values correspond to the three intermediate quarters of the ranges of measurements defined by L .

The synthesis is performed via the segmented interpolation scheme presented in Section 2.3.6. Each synthesized mannequin is then measured with m_T (see Section 2.3.5) in order to extract the resulting tailor measurements x_t that produce its resulting geometry. Table 2.4 presents the relative error $\epsilon = \left| \frac{x_t - Me_f}{Me_f} \right| \times 100$ between the resulting (x_t) and input (Me_f) measurements. This error is intended to display the accuracy with which the measurement-driven mannequins satisfy their input measurements. Figure 2.18 presents a sample of 10 randomly selected mannequins (see Table 2.5) from the 243 measurement-driven mannequins in order to visualize variations of synthesized models.

Table 2.4: Relative error between input and real measurements in set of synthesized mannequins. Measurements performed with m_T .

	Height (<i>He</i>)	Shoulder Width (<i>Sh</i>)	Breast Perimeter (<i>Br</i>)	Waist Perimeter (<i>Wa</i>)	Hip Perimeter (<i>Hi</i>)
Average Error (%)	0.2	2.6	2.4	0.8	0.9
Maximum Error (%)	0.4	6.6	7.0	1.5	2.2
Minimum Error (%)	0.0	0.1	0.0	0.0	0.1

Table 2.5: Tailor measurements of mannequins shown in Figures 2.18 and 2.19. Measurements in cm.

Mannequin	Height (<i>He</i>)	Shoulder Width (<i>Sh</i>)	Breast Perimeter (<i>Br</i>)	Waist Perimeter (<i>Wa</i>)	Hip Perimeter (<i>Hi</i>)
(1)	153.75	35.75	101.25	102.5	134.75
(2)	153.75	35.75	118.5	102.5	117.5
(3)	153.75	41.5	135.75	102.5	117.5
(4)	153.75	47.25	118.5	122.25	134.75
(5)	159.5	41.5	118.5	82.75	117.5
(6)	159.5	47.25	101.25	82.75	117.5
(7)	165.25	35.75	101.25	82.75	117.5
(8)	165.25	41.5	101.25	122.25	117.5
(9)	165.25	41.5	118.5	102.5	134.75
(10)	165.25	47.25	135.75	122.25	117.5

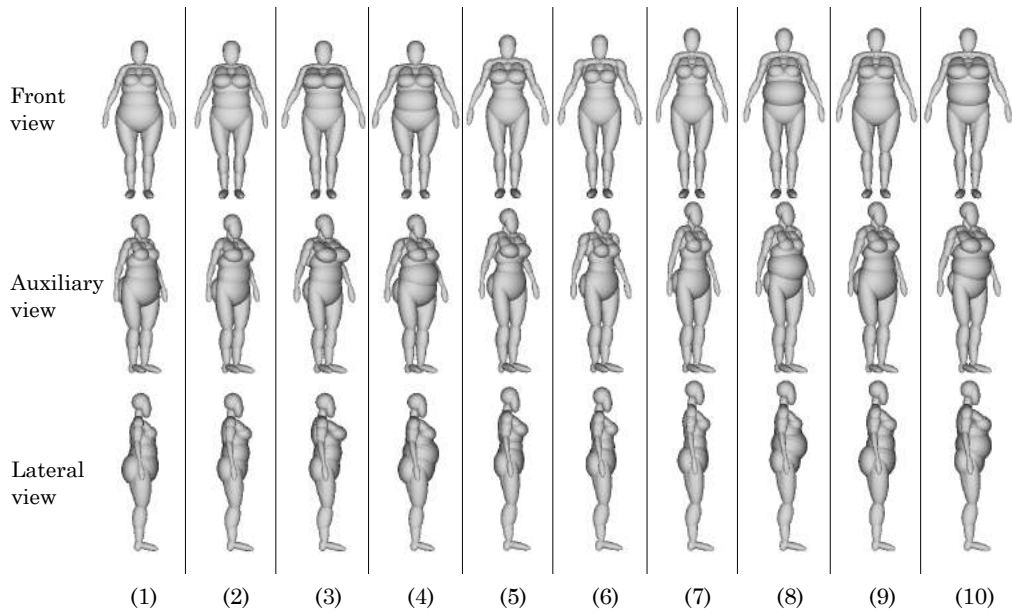


Figure 2.18: Examples of synthesized ellipsoid-based mannequins using segmented interpolation approach.

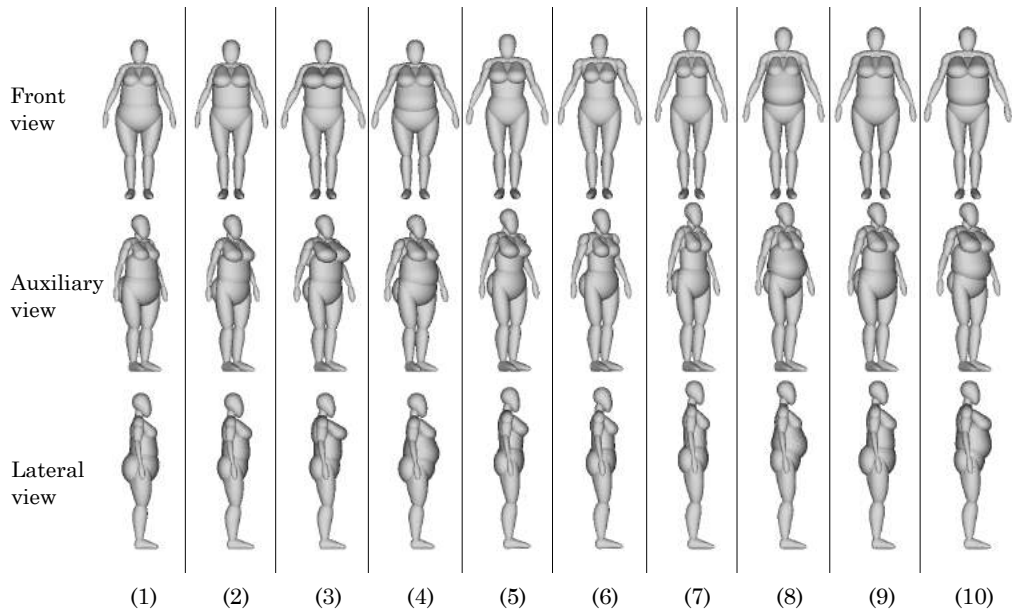


Figure 2.19: Cushion-based mannequins. These mannequins correspond to the same mannequins in Figure 2.18 with ellipsoids converted to cushions.

2.4.2 Quantitative Comparison: Cushion-Based Mannequin vs. Mesh-Based Model

We extracted the tailor measurements from a mesh-based primogenial model (see Table 2.2). These measurements served as the input and goal for the synthesis of an ellipsoid- or cushion-based mannequin. Tailor measurements were extracted from both and are compared in Table 2.6. A visual comparison can be seen in Figure 2.20.

Table 2.6: Relative error between Mesh-based Model and Cushion-based Mannequin measurements (cm). Measurements performed with m_T .

	Height (He)	Shoulder Width (Sh)	Breast Perimeter (Br)	Waist Perimeter (Wa)	Hip Perimeter (Hi)
Mesh-based Model	170	42.8	99.8	72.5	99.7
Cushion-based Mannequin	170.4	43.3	104.2	67.2	97.2
Error (%)	0.2	1.2	4.4	7.3	2.5

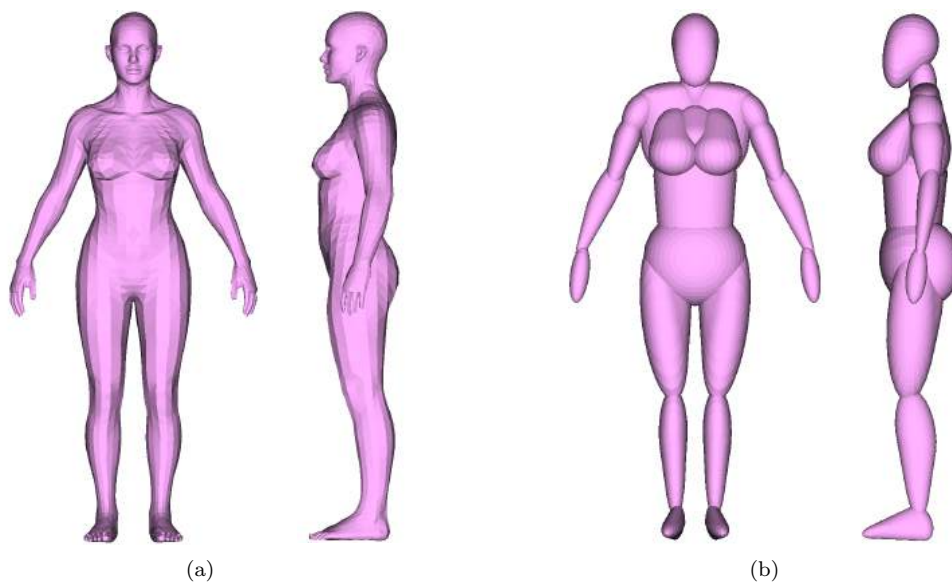


Figure 2.20: Visual comparison of Mesh-based Model vs. Cushion-based Mannequin synthesized using the measurements from the Mesh-based Model. (a) Mesh-based Model. (b) Cushion-based Mannequin.

2.4.3 Interaction Simulation between Convex Volume Model and Garment

We performed two soft-body (garment) vs. rigid-body (measurement-driven mannequin) interaction simulations using a physics engine (Ammo.js [5]). These simulations were executed in real-time and are intended to exhibit the usefulness of the convex-volume-based measurement-driven mannequins in garment-fitting simulation. The two simulations can be seen in Figures 2.21 and 2.22, in which it is visible that the garments fit the shape of the mannequins.

Since the mannequins are already sets of convex volumes, no convex decomposition is required for collision detection, avoiding additional processing steps. Specific details of the configuration of the physics engine, the soft-body, and the rigid-body are not provided since they are not relevant to the focal point of this manuscript. This manuscript's purpose is to present the modeling scheme for the measurement-driven mannequins, not to design garments nor to specify their interaction with the mannequins. Further research will focus on applications using the mannequins, such as garment-fitting simulation and its details.

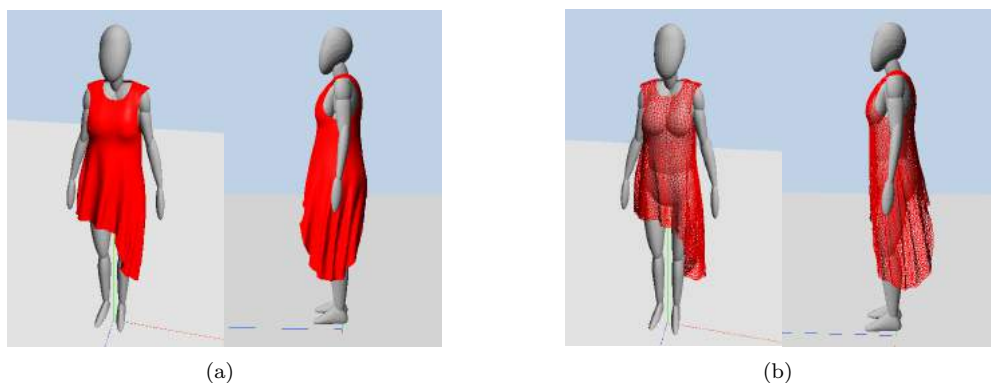


Figure 2.21: Interaction simulation of Slim Tall model and garment using cushion model and showing rigid-body vs. soft-body interaction. Visualization: Constructed by us in Three.js [41]. Simulation: Constructed by us in Ammo.js [5]. (a) Solid-color garment. (b) Wireframe garment.

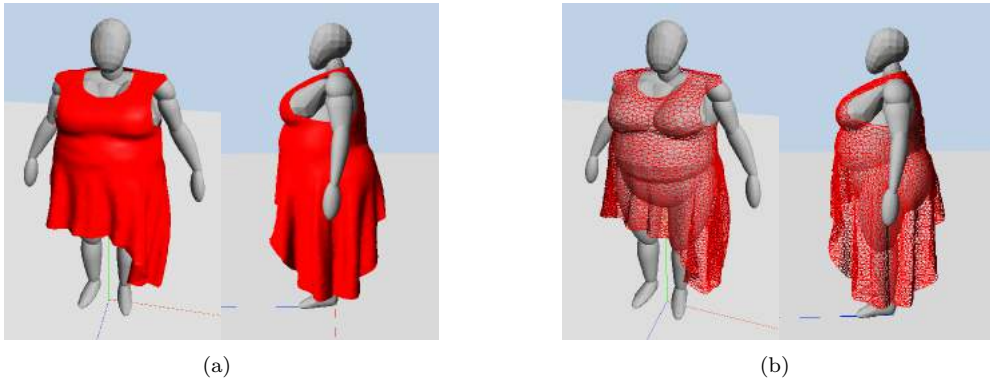


Figure 2.22: Interaction simulation of Chubby Small model and scaled garment using cushion model and showing rigid-body vs. soft-body interaction. Visualization: Constructed by us in Three.js [41]. Simulation: Constructed by us in Ammo.js [5]. (a) Scaled garment. (b) Wireframe scaled garment.

2.5 Conclusions and Future Work

This manuscript presents a parametric modeling scheme for digital mannequins that represents the female human body as a set of convex volumes. Such a scheme allows synthesis of mannequins that satisfy the specified (input) tailor measurements with an average deviation of 1.5%, as presented in Table 2.4. The aforementioned hold a reasonable and realistic demeanor. The scheme also allows a wide variety of phenotypes across different ethnic groups to be approximated without any athletic idealization (see Figure 2.18).

The proposed modeling scheme contrasts with those found in the literature due to our mannequins being created with convex volumes as opposed to non-convex meshes (see Section 2.2). This results in our method holding the following advantages: (1) reduced computational costs and data storage; (2) reduced tuning for parameterization due to the small number of parameters used; (3) since the ellipsoids have attached coordinate systems (as robotic limbs), our formulation opens opportunities for straightforward motion modeling; and (4) no need for recomputing surface (skin) for pose definition. In addition, the mannequins are shown to be economical for garment-fitting simulation. This is due to the fact that the processing steps needed for preparing non-convex models for garment-fitting simulation (collision detection) [42–48] are avoided by already having a set of convex volumes.

Notice that our approach produces a gross approximation of pose and demeanor of the digital mannequin by using a set of convex primitives (whose boolean union is obviously non-convex). On the other hand, the existing literature uses detailed triangular meshes to express the mannequin. This difference in intention (coarse vs. detailed shapes) prevents a fair numerical comparison between our method and existing methods.

Future work is encouraged to define motion modeling (pose definition). Moreover, it is encouraged to extend the convex volume modeling scheme to model male human bodies and to expand the set of measurements (e.g., including crotch length) that define parameterization. It is important to keep in mind that this manuscript already achieves a wide variety of mannequins with a reduced number of parameters. Adding more measurement parameters will allow for the creation

of more-intricate mannequins but will require more tuning.

Our convex (ellipsoid or cushion) volume approximation of a 3D female humanoid avoids explicit computation of the humanoid skin. When the humanoid changes pose, the convex components can be repositioned via their attached $SO(3)$ coordinate frame. If needed, the skin of the humanoid may be computed via alpha-shape approaches for the current humanoid instead of modifying a hypothetical skin of the previous humanoid. Figure 2.23 displays a hint for skin computation (using Blender™) for our convexly decomposed humanoid. We point out that this initiative *is not* the aim of the present manuscript, rather for future ones.

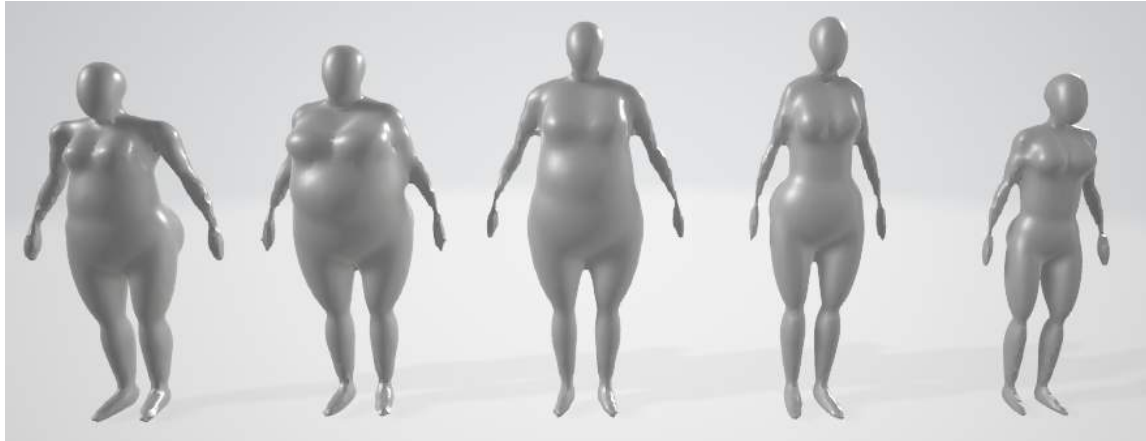


Figure 2.23: Smooth representations of the Cushion-based Mannequins. These representations *are not* the aim of the present manuscript, rather for future ones.

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Abbreviations

The following abbreviations are used in this manuscript:

Term	Description
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Me	A set of tailor measurements $Me = [He, Sh, Br, Wa, Hi]$ that describes the coarse shape and size of a female body.
He	Height.
Sh	Shoulder width.
Br	Breast perimeter.
Wa	Waist perimeter.
Hi	Hips perimeter.
C	Cushion. 2-manifold mesh surface in \mathbb{R}^3 . Computed as the convex hull of two ellipsoids (which can be the same) positioned and oriented arbitrarily in space.
SO(3)	Special Orthogonal Group.
RHCCS	SO(3) Right Handed Canonical Coordinate System.
S	4×4 homogeneous matrix. SO(3) Right Handed Canonical Coordinate System (RHCCS). Defines the position and orientation of an ellipsoid in \mathbb{R}^3 .
D	Point in \mathbb{R}^3 . $D_i > 0$, $i = 1, 2, 3$. Defines the measurements of the semi-axes of an ellipsoid in \mathbb{R}^3 .
A	A set of points in \mathbb{R}^n . Different sets of tailor measurements.
x	An element from A containing a set of particular tailor measurements. $x \in A$. An instance of Me . $x = [He, Sh, Br, Wa, Hi]$
L	A set of n ordered pairs that define the upper and lower limits of the components of the points $x \in A$.
B	A set of ellipsoids in \mathbb{R}^3 that approximates the shape and size of a female human body. B satisfies a particular set of tailor measurements $x \in A$. Each ellipsoid in B is described by a particular S and D (geometry). B is conformed of topology and geometry data. Synthesized mannequins B are displayed in gray color.
H	A set of different B 's that approximate the shape and size of different female human bodies. Each $B_i \in H$ is described by the measurements of a specific point $x_i \in A$.
RM	List of n tuples representing the Reference Mannequins. $RM = [(B_1, Me_1), (B_2, Me_2), \dots, (B_n, Me_n)]$. $RM \subset H$. With B_i an ellipsoidal model (geometry data) that satisfies the measurements in Me_i , with $i = 1, 2, \dots, n$. Each Me_i is defined by a combination of the values of L .
m_T	Set of functions $m_T : H \rightarrow A$. Set of heuristics to obtain the tailor measurements of a digital model B .
$F(Me)$	Set of synthesis functions $F : A \rightarrow H$. A particular m_T^{-1} . Set of functions that produce a digital mannequin B that satisfies a set of measurements Me based on known data points RM . Weighted average of the form of Eq. 2.1.
3D mannequin	3D digital model that approximates the female human body as a set of convex volumes (ellipsoids and cushions).
3D model	3D non-convex mesh that represents the female human body.
BM	Base mannequin. 3D mannequin instance. Template mannequin used to construct RM

3

Conclusions

This thesis presents a novel method for the synthesis of human 3D mannequins as a family of ellipsoids and cushions (i.e convex hull of two ellipsoids), given a set of tailor measurements. The results of such method show the successful creation of arbitrary mannequins that satisfy their desired measurements with an average deviation of 1.5%. Therefore, the method proves to be an accurate, fast, and cost-effective alternative for the creation of digital mannequins. In addition, the synthesized mannequins exhibit their usefulness in garment-fitting simulation applications.

Finally, the different contributions presented here can be further extended. Therefore, future research can be focused on: (1) extending the ellipsoid-based modeling approach to synthesize male mannequins. (2) Defining a parametrized motion modeling scheme for the synthesized mannequins.

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